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Strain-engineered divergent electrostriction in KTaO_3

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We investigate the electrostrictive response across a ferroelectric phase transition from first-principles calculations and show that M , the field-induced electrostrictive tensor, controlling the amplitude of the electric-field induced strain, can be made arbitrarily large through strain engineering. We take as a case study the epitaxial strain-induced transition from para- to ferro-electricity of KTaO_3 . We show that the magnitude of the field-induced electrostriction diverges with the permittivity at the transition, hence exhibiting giant responses through a calculation of both the M and Q electrostrictive tensors. We explain the origin of this giant electrostrictive response in KTaO_3 using a microscopic decomposition of the electrostriction coefficients, and use this understanding to propose design rules for the development of future giant electrostrictors for electromechanical applications. Finally, we introduce a further means to calculate electrostriction, specific to ferroelectrics, and not yet utilised in the literature.

Electrostriction is an electromechanical coupling present in all dielectrics which describes the quadratic induction of a strain or stress, due to an electric or polarisation field. Despite its ubiquity, it is often dwarfed in amplitude by its linear counterpart, piezoelectricity, which constitutes the primary response in most electromechanical systems. However, renewed interest in electrostriction has grown due to the recent discovery of materials which exhibit "giant" electrostrictive responses,^[1–3] capable of competing with piezoelectrics in terms of responses. These electrostrictors exhibit a host of attractive advantages over piezoelectrics such as: (i) minimal hysteresis in the strain-field response, (ii) increased stability of induced deformations, (iii) smaller response time, (iv) enhanced temperature stability, and (v) materials which are lead-free and environmentally friendly.^[4–6]

In ferroelectric materials, there is a consensus that the large electromechanical response of ferroelectric materials is mostly due to their piezoelectric rather than electrostrictive response. Additionally, it is often accepted from experimental studies^[5–7] and phenomenological treatment^[8] that the electrostriction remains relatively small and unchanged across ferroelectric phase transitions. However, these studies report the electrostrictive Q_{ijkl} coefficient (relating strain to the polarisation squared) while a few reports^[9, 10] found that the electrostrictive M_{ijkl} tensor (relating strain to the electric field squared) increases rapidly with temperature together with the permittivity near phase transitions. However, it is believed that the M_{ijkl} response is nevertheless negligibly small with respect to the piezoelectric response, and therefore useless in terms of technological applications^[11]. Hence, the question remains of whether inducing phase transitions where the permittivity diverges enables to increase the electrostrictive response significantly enough to make electrostriction in-

teresting for electromechanical applications.

In this Letter, through a thorough examination of electrostriction at the strain-induced ferroelectric phase transition (FEPT) in KTaO_3 from first-principles calculations, we demonstrate a giant electrostrictive response can indeed be obtained in ferroelectric materials at the phase transition, confirming that, though the components of the polarisation tensor Q do not change much, the out-of-plane electric-field tensor components diverge and reaches values that make electrostriction interesting for electromechanical applications. In addition, through a microscopic decomposition of the electrostriction tensors, we show that it is the soft transverse optical mode that is responsible for the large electrostriction.

To proceed, we note that while one may consider electrostriction as the "strain/stress induced quadratically by an electric/polarisation field", one may also view it as the thermodynamically equivalent "linear change in susceptibility/inverse susceptibility induced by a stress or a strain"^[12, 13] shown below:

$$\begin{aligned} \frac{1}{\epsilon_0} \frac{\partial \eta_{ij}}{\partial X_{kl}} &= -2Q_{ijkl} & \frac{1}{\epsilon_0 \epsilon_0} \frac{\partial \eta_{ij}}{\partial x_{kl}} &= 2q_{ijkl} \\ \epsilon_0 \frac{\partial \chi_{ij}}{\partial X_{kl}} &= 2M_{ijkl} & \epsilon_0 \frac{\partial \chi_{ij}}{\partial x_{kl}} &= -2m_{ijkl}. \end{aligned} \quad (1)$$

See the supplemental material for details of the thermodynamical derivation of these equations.^[14] In our previous work^[13], we outlined the advantages of this method of calculation, amongst which are greater computational efficiency and robustness.

Viewed from the perspective of Eqs.(1), we see that at a strain- or stress-induced phase transition, involving the divergence of the susceptibility, *some* electrostrictive tensor components *must* become large.^[15] To compute Eqs. (1) we have used the DFT package ABINIT (version 8.6.1)^[16], with k-point grid densities of $8 \times 8 \times 8$ and a plane wave cutoff energy of 75 Ha, to ensure

convergence of electrostrictive coefficients of about 1%. The PseudoDojo [17] normconserving pseudopotentials were used, and the exchange-correlation functional was treated using the generalised gradient approximation of Purdue, Burke, and Ernzerhof, modified for solids (PBEsol). [18] We note that obtaining the electrostriction tensors in this manner using eq.1 and finite differences, will yield an "improper" electrostriction tensor containing contributions described by Nelson and Lax [19]; the "proper" tensor may be obtained from this by the addition of permittivity components to certain electrostriction components. [13, 19]

As a test case, we will analyse the electrostrictive response at the strain-induced FEPT present in KTaO_3 . KTaO_3 is a highly suitable material for such a study as it is an incipient ferroelectric which undergoes a ferroelectric phase transition due to relatively small axial stress. A FEPT is reported at 0.6 GPa by Uwe [7] and for a strain of 1% by Tyunina [20] at low temperature (4.2 K), which can be studied experimentally on single crystals or epitaxial thin films. In addition, KTaO_3 has a wide range of applications [20–24], including the recent discoveries of superconductivity [22, 23] or dynamic multiferroism [24], making it a highly technologically relevant material.

We present in Table I our calculated ground state properties of KTaO_3 along with previous PBEsol calculations from the literature, as well as experimental measurements. We obtain a bandgap in good agreement with previous PBEsol theory, but it is underestimated with respect to the experimental values as expected from the PBEsol functional, though we can reproduce the indirect gap from R point to Γ -point. For the lattice and elastic constants good agreement is obtained with both experiment and previous theory. While no previous experimental or theoretical works have determined the M_{ijkl} electrostrictive coefficients, for the Q_{ijkl} coefficients, we obtain reasonable agreement with previous experiment [6, 7], with the disagreement between our computed values and the experimental ones being equivalent to the variances amongst the experimental values.

To investigate electrostriction through the FEPT, we have calculated the properties of KTaO_3 over a range of biaxial compressive and tensile strains from -0.7% to 0.7%, as may be achieved through epitaxial growth on various substrates. This was done by imposing the strain components $x_{11} = x_{22} = (a_s - a_0)/a_0$ where a_0 is the relaxed lattice constant of KTaO_3 and a_s is the lattice constant of the substrate, and by relaxing the z direction of strain.

In the top part of Fig. 1 we show the impact of these various epitaxial strains on the permittivity tensor. Consistent with previous works on KTaO_3 , the epitaxial strain induces a FEPT [7, 20], and we see it is in fact the tensile strains which drive the polar displacement. On the left, the middle panel reveals that the tensile strain induced in the z -direction by the compressive epitaxial xy

Coefficient	Present Calc	Lit Calc	Exp
$E_g^{R-\Gamma}$ (eV)	2.16	2.14 ^c	4.35 ^f
$E_g^{\Gamma-\Gamma}$ (eV)	2.77	2.70 ^d	3.64 ^f
a_0 (Å)	3.9817	3.989 ^c	3.9885 ^e
C_{11} (GPa)	453.2	474.7 ^c	431 ^g
C_{12} (GPa)	76.8	62.752 ^c	103 ^g
C_{44} (GPa)	99.7	197.10 ^c	109 ^g
ω_{TO1}	63	104.01 ^h	85 ⁱ 81 ^j
ω_{LO1}	171	173.08 ^h	185 ^j
ω_{TO2}	180	179.57 ^h	198 ⁱ 199 ^j
ω_{LO2}	398	392.64 ^{h*}	
$\omega_{TO3} = \omega_{LO3}$	256	237.7 ^h	279 ^j
ω_{TO4}	529	561.33 ^h	556 ⁱ 546 ^j
ω_{LO4}	791	821.49 ^h	826 ^j
ϵ	433		
Q_{11} (m^4C^{-2})	0.1256	-	0.087 ^a
Q_{12} (m^4C^{-2})	-0.0313	-	-0.023 ^a
Q_h (m^4C^{-2})	0.063	-	0.041 ^a , 0.052 ^b
M_{11} (m^2V^{-2})	1.98×10^{-18}	-	-
M_{12} (m^2V^{-2})	-4.70×10^{-19}	-	-
M_h (m^2V^{-2})	1.05×10^{-18}	-	-

TABLE I. Bulk paraelectric ground state KTaO_3 electronic, structural, elastic, and electrostrictive properties obtained via calculation and measurement. a=Ref[7]; b=Ref[6]; c=Ref[25]; d=Ref[26]; e=Ref[27]; f=Ref[28]; g=Ref[29]; h=Ref[30]; i=Ref[31] (soft mode at 300K, others at 10K); j=Ref[32] (RT). *In ^h the LO2 mode is mislabeled as the TO3 mode due to the fact that LO2 is higher in frequency than the non polar TO3 and LO3 modes.

strain leads to the softening of the transverse optic (TO) mode polar in z , and a divergence of ϵ_{33} , with the FEPT occurring at 0.4% epitaxial xy strain; on the right, the epitaxial tensile strain leads to the simultaneous softening of the polar TO modes in x and y , and a divergence of ϵ_{11} and ϵ_{22} , with the transition occurring at around 0.26% epitaxial strain. This earlier transition point is due to the fact that in this case the tensile strain is being directly imposed on the x and y coordinates, whereas with the compressive strain, the tensile strain in the z -direction occurs more slowly due to a Poisson effect. This occurrence of the FEPT at the rather small compressive and tensile strains of 0.4 and 0.26% is consistent with the incipient nature of the FE in KTaO_3 .

The bottom panel of Fig. 1 shows that the electrostrictive tensor components M_{33} and M_{13} also diverge at the FEPT, contrary to reports in the literature that electrostriction is constant at a phase transition [33]. To compute the electrostriction, at each fixed epitaxial strain, we apply a further strain in the z -direction, of magnitude of -0.005 , to the already relaxed c lattice vector, and calculate again the permittivity using DFPT. The coefficient m_{33} is obtained from the derivative of ϵ_z with respect to the applied x_{33} ; and the rate of change of ϵ_x w.r.t. x_{33} yields the coefficient m_{13} . The technologically relevant M_{33} and M_{13} , are then derived by appropriate consideration of the epitaxial boundary con-

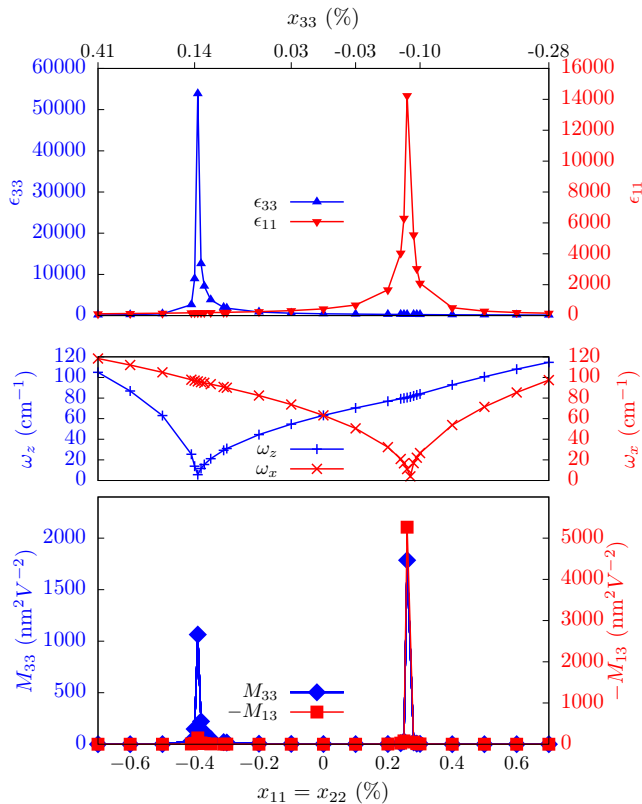


FIG. 1. Variation of with epitaxial strain ($x_{11} = x_{22}; X_{33} = 0$) of: permittivity tensor components ϵ_{11} and ϵ_{33} (top); lowest x and z polar phonon modes, ω_x and ω_z (mid); and electrostriction tensor components M_{33} and M_{13} (bottom). Compressive epitaxial strain induces a tensile strain induced phase transition in the z-direction, and tensile epitaxial strain induces a phase transition in the x=y direction.

ditions. With:

$$\begin{aligned} M_{33} &= 2s_{12}m_{13} + s_{33}m_{33} \\ M_{13} &= (s_{11} + s_{12})m_{13} + s_{13}m_{33}, \end{aligned} \quad (2)$$

where s_{ij} are elastic susceptibilities, for which we have used the equilibrium values, noting that epitaxial strains of $< \pm 1$ are unlikely to induce significant elastic nonlinearities [34].

Focusing first on the compressive epitaxial strain induced transition (at -0.4%), we observe spikes in both M_{33} and M_{13} ; with M_{33} reaching $1 \times 10^{-15} \text{ m}^4/\text{C}^2$, a value rarely observed except for some polymers, and M_{13} reaching the smaller, though still considerable value of $-1.5 \times 10^{-16} \text{ m}^4/\text{C}^2$. This means that in a compressively strained epitaxial layer, an electric field will produce a significant tensile strain in the z-direction, and also a compressive strain parallel to the plane of the layer. To put this in context, the peak M_{33} is equivalent to an *effective* piezoelectric coefficient of $d_{33}^{eff} = 60,000 \text{ pm/V}$, which compares very favourably with d_{33} of up to 600 pm/V [35] values in classic piezoelectric material

PZT. This large tensile z-strain could have applications in micro-fluidics, adjustable mirrors etc., where the lead-free nature of KTaO_3 makes it particularly attractive when compared with other lead-containing materials.

Looking at the tensile-strain-induced transition (at 0.26%), we find again a divergence of the coefficients, though this time both reaching much higher values, with M_{13} reaching $-5 \times 10^{-15} \text{ m}^4/\text{C}^2$, and M_{33} reaching $2 \times 10^{-15} \text{ m}^4/\text{C}^2$. In this case an electric field in z will produce considerably more strain in-plane/xy than in the case of compressive epitaxial strain.

Figure 1 thus demonstrates that electrostriction in lead-free KTaO_3 , brought near the phase transition through epitaxial growth on an appropriate substrate, may be an ideal active material candidate for future electromechanical devices. In addition, we note that the values obtained of the order of $10^{-15} \text{ m}^4/\text{C}^2$, compare very favorably with known giant electrostrictors, such as (Nb,Y)-doped Bi_2O_3 ($M \approx 10^{-17} \text{ m}^4/\text{C}^2$) [36], Gd-doped ceria ($M \approx 10^{-17}$ to $10^{-16} \text{ m}^4/\text{C}^2$) [37] and $\text{La}_2\text{Mo}_3\text{O}_9$ ($M = 1.5 \times 10^{-18} \text{ m}^4/\text{C}^2$) [38] without being restricted to low frequencies.

To better understand this giant electrostriction, we can profit from the particular manner in which the methods based on eqs.1, and introduced in Ref.13, determine the electrostrictive coefficients. Through the decomposition of the permittivity tensor into its mode by mode contributions, we are also able to decompose the electrostriction tensor. This decomposition is illustrated for the ϵ_x, ϵ_z and the electrostriction tensor components m_{33} and m_{13} in Fig. 2. The figure shows that all four TO modes contribute to ϵ_{11} and m_{13} , whilst only three contribute to ϵ_{33} and m_{33} . However, amongst all of these contributions, the only that matter near the transitions are those of the soft TO1 modes, with all others being negligible and indistinguishable from zero in the plot. We note also that in Fig. 2, the behaviour of the m_{ij} is much simpler than that of the corresponding M_{ij} shown in the bottom panel of Fig. 1, with m_{33} and m_{13} each exhibiting only one peak; however, we see that it is the mixing of these coefficients, according to Eq.2, which leads to the double peaked M_{ij} .

To clarify why some previous experimental observations reported that the Q electrostrictive response is constant across FEPT,[6] we have also examined the evolution of the Q_{33} coefficient of our strained KTaO_3 . Figure 3 shows the development of η_{33} and Q_{33} at the compressive strain induced phase transition. We plot η_{33} as the Q_{33} is obtained by its derivative w.r.t. the compressive z-strain. Contrarily to the permittivity and M_{33} , a regular, non-divergent behaviour for both η_{33} and Q_{33} . In fact, when approaching the FEPT at -0.4% epitaxial strain, the coefficient Q_{33} evinces a constant behaviour, and whilst the coefficient decreases as the compressive strain increases beyond the transition, it is a very small change, i.e. $< 3\%$ over the considered strain range.

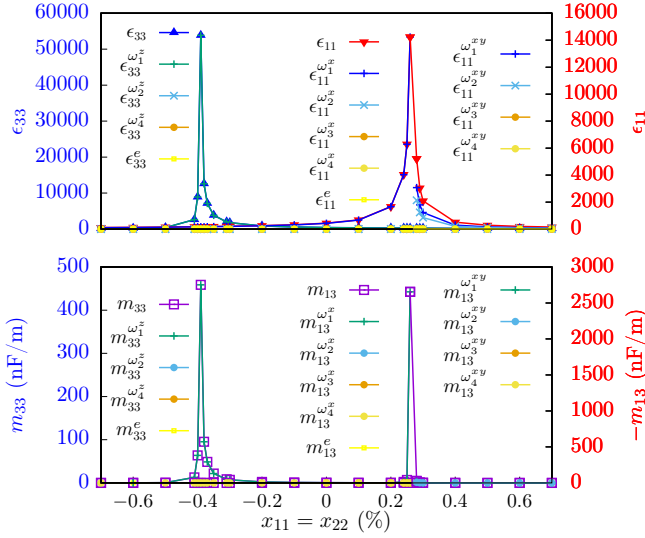


FIG. 2. Decomposition of (top) permittivity tensor components ϵ_{33} and ϵ_{11} , and (bottom) electrostrictive tensor components m_{33} and m_{13} into their mode by mode and electronic contributions. For both the permittivity and electrostriction, the primary contribution is from the softening TO mode.

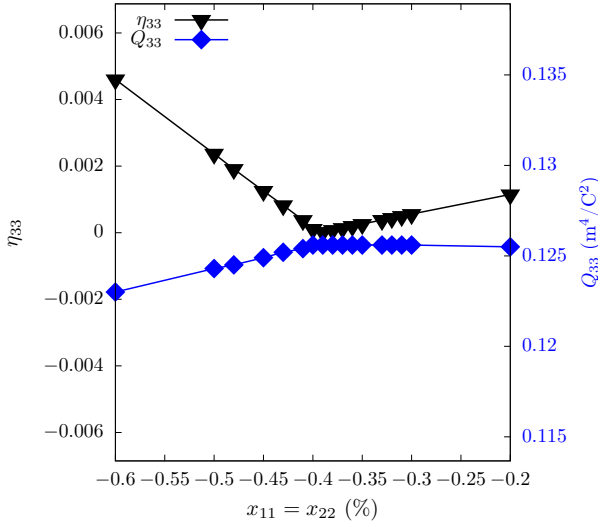


FIG. 3. η_{33} and Q_{33} plotted against epitaxial strain. Q_{33} is obtained by applying a further z-strain of -0.05% at each epitaxial strain and computing the rate of change of ϵ_{33} with respect to stress. See text.

It might look surprising that the M_{33} electrostrictive coefficient diverges at FEPT while the Q_{33} is almost unaffected but this makes sense when we consider eqs. (1), as $\eta = 1/\chi$ where we have that $Q = -1/\chi^2 \partial\chi/\partial X$. Hence, the diverging susceptibility (i.e. large $\partial\chi/\partial X$) is compensated by the $1/\chi^2$ part such that they balance each other out to give a nearly constant Q coefficient at the FEPT, while the M coefficient is directly proportional to $\partial\chi/\partial X$ and increases with it. Therefore, whether or not elec-

trostriction is claimed to diverge and become huge at the FEPT [9] or not [6, 7] depends on whether one analyses the M and m coefficients (which *must* diverge), or the Q and q coefficients (which do not) for continuous transitions.

Finally, we demonstrate that the ferroelectric phase offers a unique approach to the calculation of the electrostrictive coefficients, not yet implemented in DFT. This is based on the relation of the electrostriction tensor to the spontaneous polarisation and piezoelectricity tensor:[12][39]

$$g_{ijm} = 2Q_{ijmn}P_n, \quad (3)$$

where g_{ijm} is the piezoelectric tensor which describes the linear coupling of strains to polarisations. This means that in the range of strain where KTaO_3 is ferroelectric (below -0.4%), we can determine the Q coefficient through the spontaneous polarization (calculated through the Berry phase method) and the piezoelectric coefficient (directly accessible from DFPT). Just below the critical strain for FEPT (-0.4%), we obtained a spontaneous polarisation of $P_3 = -1.57 \mu\text{C}/\text{cm}^2$ and a piezoelectricity tensor components g_{33} and g_{31} of -4.015 and $1.035 \cdot 10^{-3} \text{m}^2/\text{C}$, respectively. Using eq. (3), this yields to $Q_{11} = 0.1278 \text{m}^4\text{C}^{-2}$ and $Q_{12} = -0.03295 \text{m}^4\text{C}^{-2}$, in good agreement with the Q values of 0.1278 and $-0.02986 \text{m}^4\text{C}^{-2}$, evaluated at the same point using eqs.1. This method to obtain the Q_{ijkl} coefficients has advantages over both the methodology we have presented in Ref.13, and the finite field methodologies found in the literature [40–42], the primary amongst which is that no finite differences or relaxations were required, just the ground-state based Berry phase and DFPT calculations. It also circumvents issues associated with applying an electric field to the paraelectric phase of a perovskite [40], and more general shortcomings associated with finite field methodologies [13].

In conclusion, we have performed a thorough investigation of electrostriction at the ferroelectric phase transition. We have outlined a route towards giant electrostriction through epitaxial strain engineering, demonstrating an electrostrictive M_{33} coefficient equivalent to an effective d_{33} coefficient of $60,000 \text{pm}/\text{V}$. The magnitude of this response, the ease with which the studied system may be grown, and the advantages of lead-free electrostrictive materials over piezoelectric materials more generally mark this as a significant scientific and technological advancement. In addition, through our treatment of both the Q_{ijkl} and M_{ijkl} tensors, we underline that whether one will observe a diverging and giant electrostriction, or a relatively constant and stable response, depends on whether one measures the Q or the M tensor. Finally, we have introduced a new method by which electrostriction may be computed in a ferroelectric using only the Berry phase technique and DFPT, without the need for relaxations or finite differences. Our results also

question if the origin of giant electrostriction [43] e.g. in LAMOX, doped ceria, or Bi_2O_3 , is coming from an intrinsic softening of a polar mode, like in KTaO_3 or if its due to intrinsic electronic effects or other extrinsic effects. This will require further experimental and theoretical researches to further understand giant electrostrictors.

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